



HARDENING

Jiří Plešek

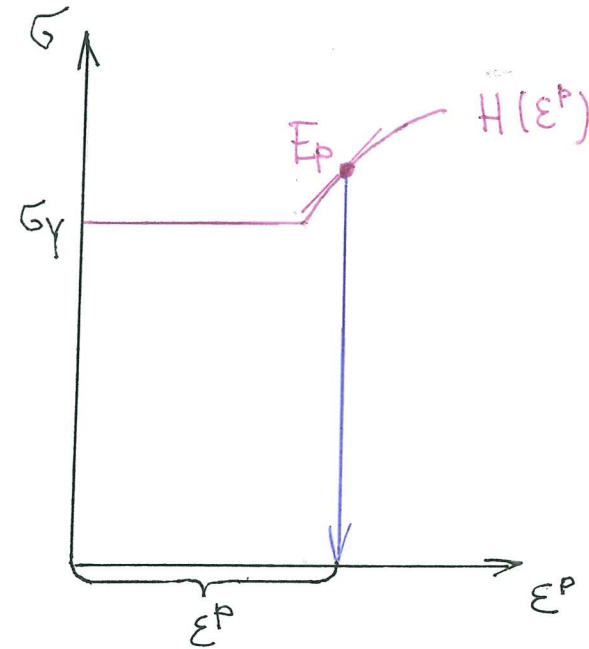
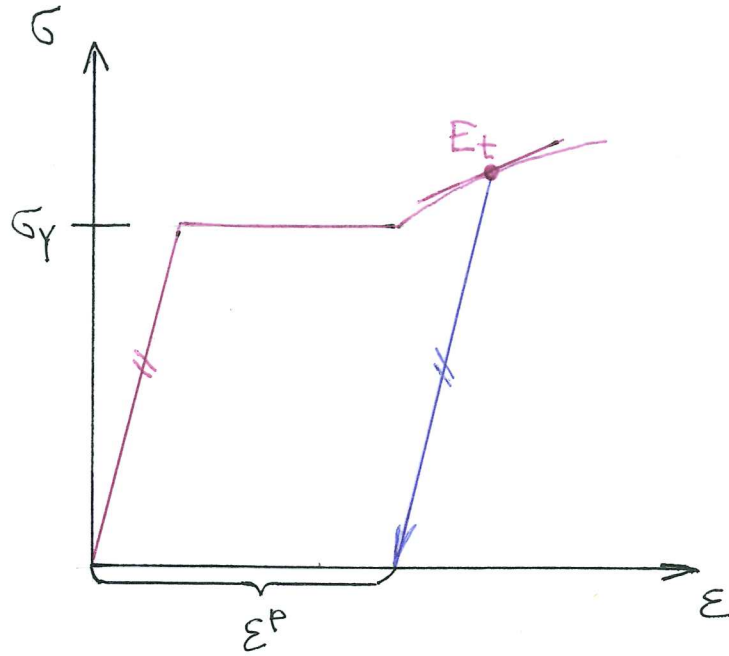
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Uniaxial hardening





Plastic modulus

Hardening function

$$H(\epsilon^p) \geq \sigma_Y, \quad H(0) = \sigma_Y, \quad E_p = H'(\epsilon^p)$$



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It holds that $E_t < E$ and $E_p \rightarrow \infty$ as $E_t \rightarrow E$, which causes some ill-conditioning for smooth σ - ϵ curves. Progressive hardening $E_t > E$ is prohibited. Perfect plasticity is recovered for $E_t = 0$.



Equivalent plastic strain

Effective strain rate

$$\dot{\epsilon}_p = \sqrt{\frac{2}{3} \dot{\epsilon}_{ij}^p \dot{\epsilon}_{ij}^p}$$



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$$\epsilon_p = \int_0^t \dot{\epsilon}_p d\tau \quad (\text{history dependent})$$

Remark: The latter quantity is also known as the cumulative plastic strain.



Isotropic hardening (1/2)

Hill (1950)

$$f(\sigma_{ij}) \leq H(\epsilon_p)$$



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Substitution

$$\dot{\sigma}_{ij} = C_{ijkl}(\dot{\epsilon}_{kl} - \lambda R_{kl}) \quad \text{and} \quad \dot{\epsilon}_p = \lambda \sqrt{\frac{2}{3} R_{mn} R_{mn}}$$



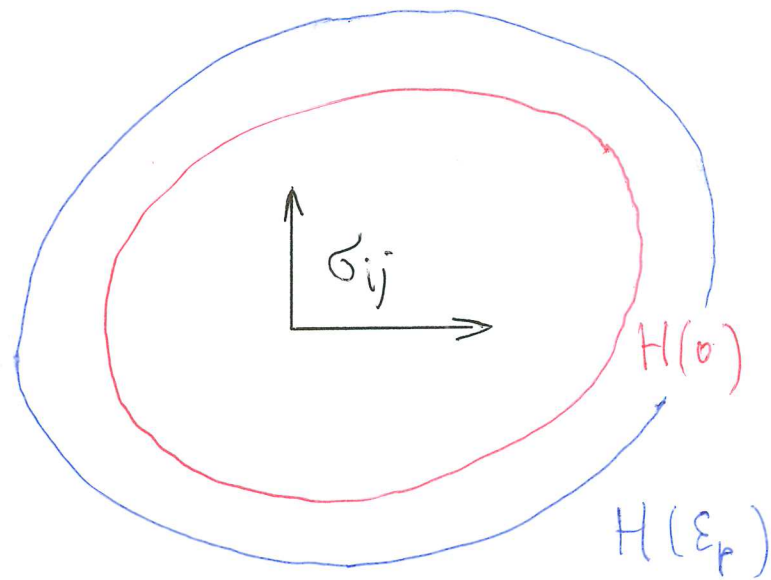
Isotropic hardening (2/2)

Plastic multiplier

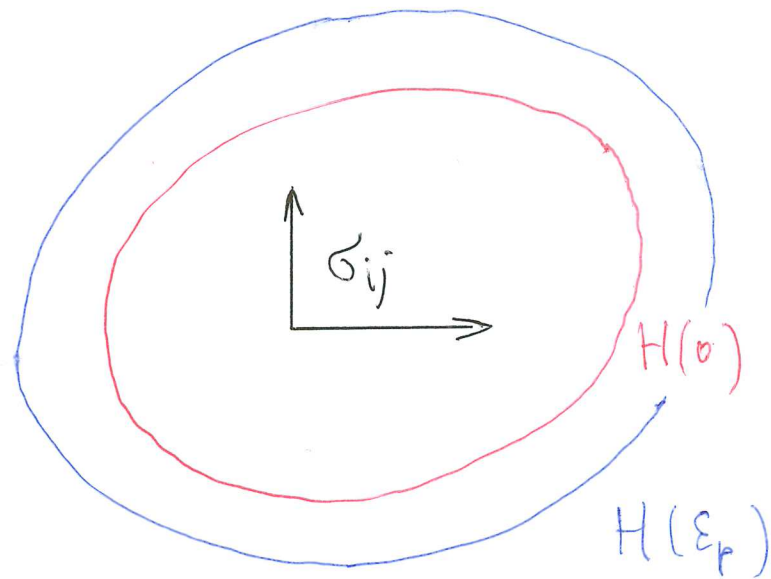
$$\lambda = \frac{\frac{\partial F}{\partial \sigma_{ij}} C_{ijkl} \dot{\epsilon}_{kl}}{E_p \sqrt{\frac{2}{3}} R_{mn} R_{mn} + \frac{\partial F}{\partial \sigma_{pq}} C_{pqrs} R_{rs}}$$

Perfect plasticity is recovered, setting $E_p = 0$.

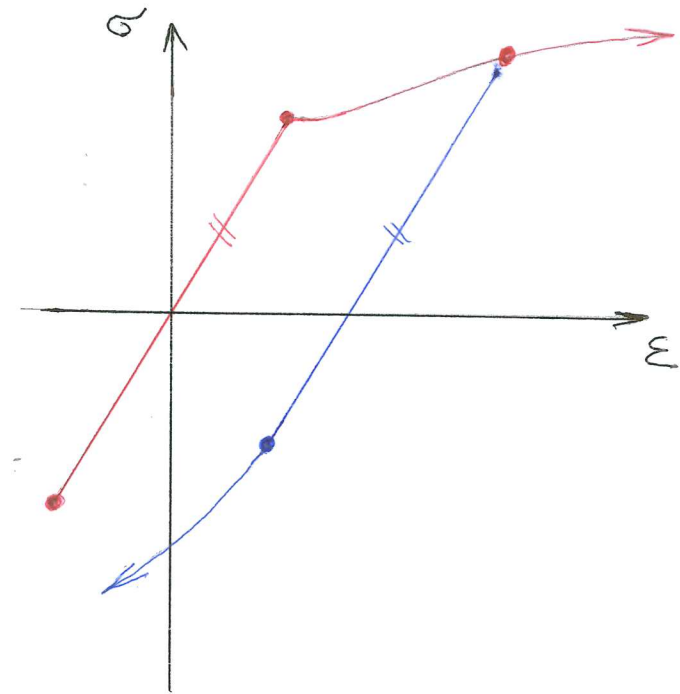
Isotropic hardening



Isotropic hardening

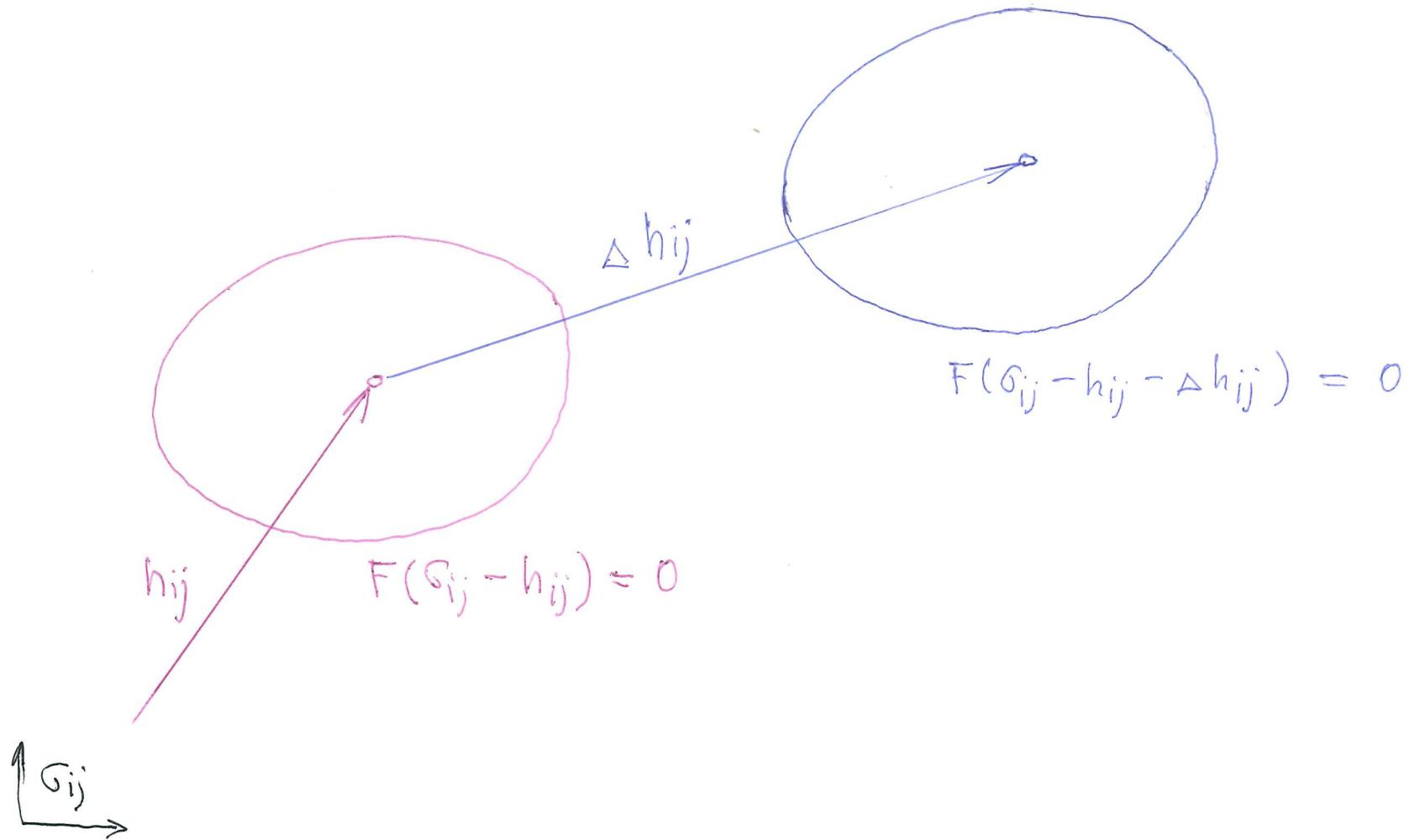


Bauschinger effect (1890)



Elastic range approximately preserved.

Kinematic hardening





Kinematic hardening (1/3)

Prager (1955)

$$f(\sigma_{ij} - h_{ij}) \leq \sigma_Y$$



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$$F(\sigma_{ij}, h_{ij}) = f(\sigma_{ij} - h_{ij}) - \sigma_Y$$



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Constitutive assumption

$$h_{ij} = c \epsilon_{ij}^p, \quad c = \text{const.}$$



Kinematic hardening (2/3)

Plastic multiplier

$$\lambda = \frac{\frac{\partial F}{\partial \sigma_{ij}} C_{ijkl} \dot{\epsilon}_{kl}}{c \frac{\partial F}{\partial \sigma_{mn}} R_{mn} + \frac{\partial F}{\partial \sigma_{pq}} C_{pqrs} R_{rs}}$$



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It must hold that $\lambda_{\text{kin}} = \lambda_{\text{iso}}$, therefore

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Associated flow rule

$$c \sqrt{\frac{\partial F}{\partial \sigma_{mn}} \frac{\partial F}{\partial \sigma_{mn}}} = \sqrt{\frac{2}{3}} E_p$$



Kinematic hardening (3/3)

J_2 -theory

$$\frac{\partial F}{\partial \sigma_{mn}} \frac{\partial F}{\partial \sigma_{mn}} = \frac{3}{2} \frac{S_{mn}}{\sigma_e} \frac{3}{2} \frac{S_{mn}}{\sigma_e} = \frac{3}{2}$$



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$$c \sqrt{\frac{3}{2}} = \sqrt{\frac{2}{3}} E_p \Rightarrow c = \frac{2}{3} E_p$$



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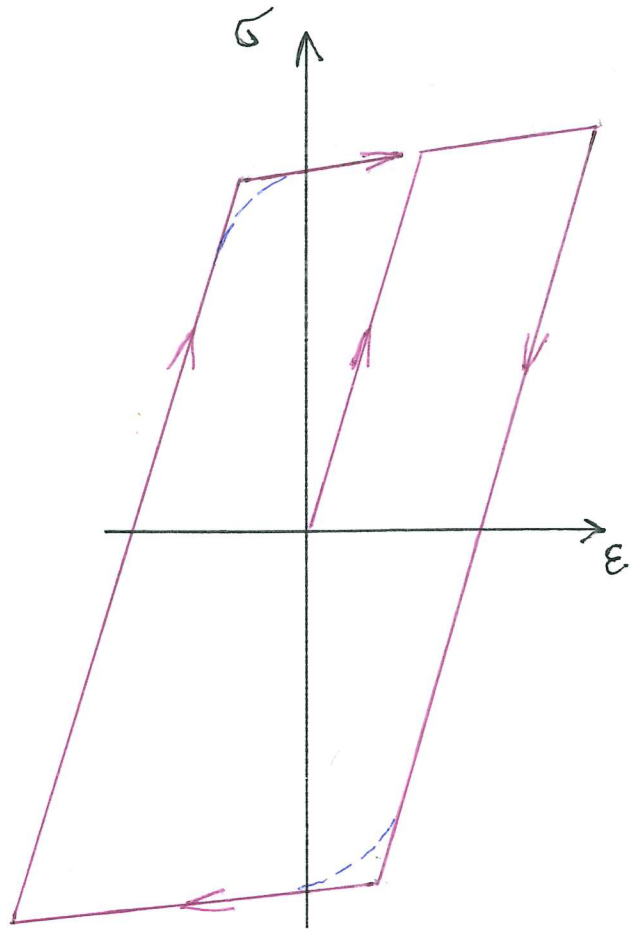
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$$c \sqrt{\frac{3}{2}} = \sqrt{\frac{2}{3}} E_p \Rightarrow c = \frac{2}{3} E_p$$

Important note: Since c is a constant, so is E_p , which implies only linear hardening is available for this particular model!

Closed kinematic cycle



(hysteretic loop)

Isotropic

+ arbitrary $H(\epsilon_p)$

- unloading

Kinematic

+ cyclic plasticity

- bilinear diagram