



# ENGINEERING PLASTICITY III

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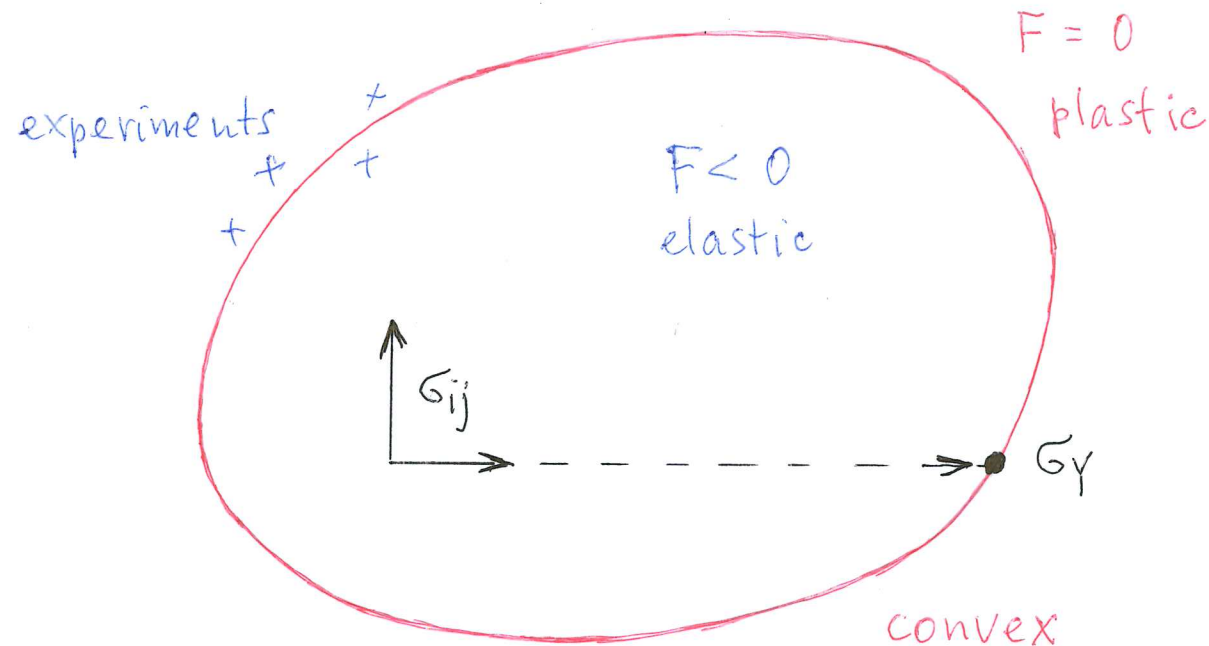
# Contents

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- Concept of yielding functions
- Effective stress
- Tresca's criterion
- Collapse of a thick wall tube

# Yield function

$$F(\sigma_{ij}) \leq 0$$



$F > 0$   
No entry!

Convexity does not follow from physics !!



# Effective stress

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## Definition

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Yield function

$$F(\sigma_{ij}) \equiv f(\sigma_{ij}) - \sigma_Y$$



# Tresca's criterion (1864)

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## 5. Validation

...Luders (1860), Schmid (1924)

Remark: Predictions can (and should) be validated.



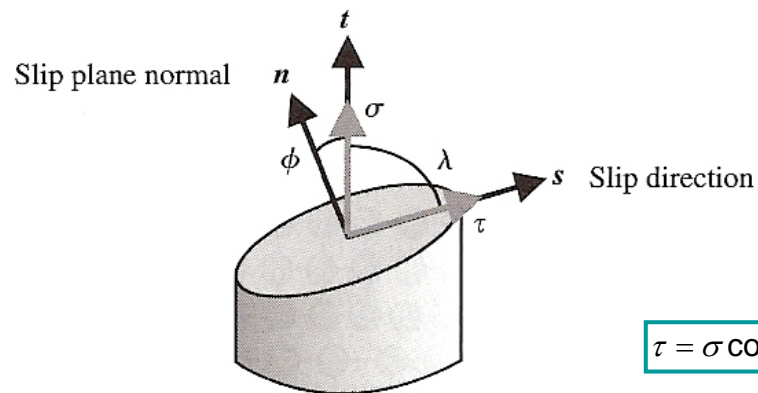
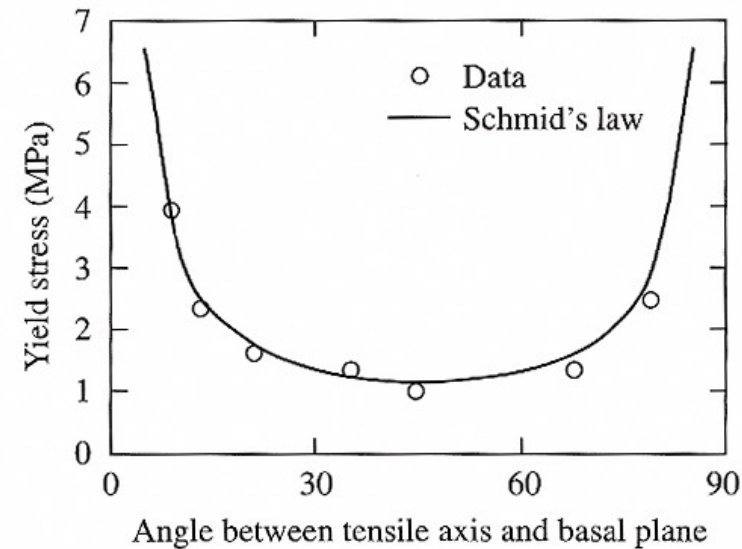
# Luders bands (1860)

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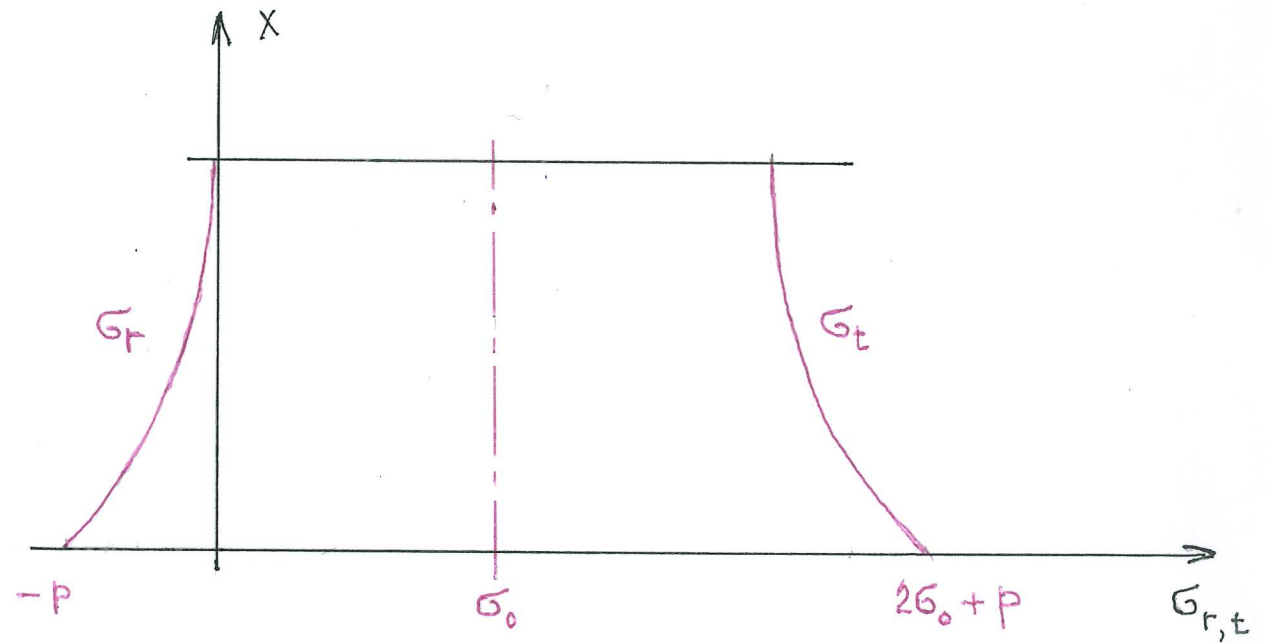
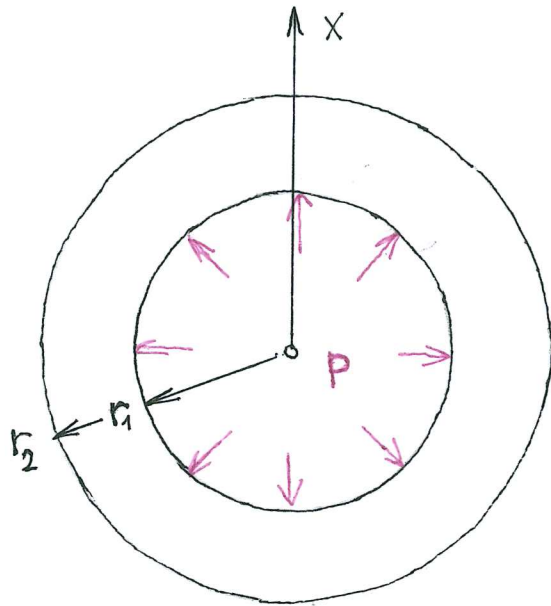
# Single crystals – Schmid's law

Metal	Structure	Slip systems	CRSS (MPa)
Cu	fcc	$\langle 1\bar{1}0 \rangle \{111\}$	0.64
Al	fcc	$\langle 1\bar{1}0 \rangle \{111\}$	0.40
Ni	fcc	$\langle 1\bar{1}0 \rangle \{111\}$	5.8
$\alpha$ -Fe	bcc	$\langle 11\bar{1} \rangle \{101\}, \langle 11\bar{1} \rangle \{112\}, \langle 11\bar{1} \rangle \{123\}$	32
Mo	bcc	$\langle 11\bar{1} \rangle \{101\}$	50
Ta	bcc	$\langle 11\bar{1} \rangle \{101\}, \langle 11\bar{1} \rangle \{112\}, \langle 11\bar{1} \rangle \{123\}$	50



$$\tau = \sigma \cos \phi \cos \lambda = \sigma (\mathbf{t} \cdot \mathbf{n})(\mathbf{t} \cdot \mathbf{s})$$

# Thick wall tube - PMD Example Manual





# Thick wall tube (1/3)

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Plastic state

$$\left. \begin{array}{l} \text{equilibrium equation: } \frac{d\sigma_r}{dx} + \frac{\sigma_r - \sigma_t}{x} = 0 \\ \text{yield condition: } \tau_e = \sigma_t - \sigma_r = \sigma_Y \end{array} \right\} \Rightarrow \frac{d\sigma_r}{dx} = \frac{\sigma_Y}{x}$$



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Solution

$$\sigma_r(x) = \sigma_Y \ln x + C$$





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Boundary condition

$$\sigma_r(r_2) = \sigma_Y \ln r_2 + C = 0 \quad \Rightarrow \quad C = -\sigma_Y \ln r_2$$



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$$\sigma_r(r_2) = \sigma_Y \ln r_2 + C = 0 \quad \Rightarrow \quad C = -\sigma_Y \ln r_2$$

Hence

$$\sigma_r(x) = \sigma_Y \ln x - \sigma_Y \ln r_2 = \sigma_Y \ln \frac{x}{r_2}$$



## Thick wall tube (2/3)

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Stress field at collapse

$$\begin{aligned}\sigma_r(x) &= \sigma_Y \ln \frac{x}{r_2} \\ \sigma_t(x) &= \sigma_Y \left( 1 + \ln \frac{x}{r_2} \right)\end{aligned}$$



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Boundary condition

$$\sigma_r(r_1) = \sigma_Y \ln \frac{r_1}{r_2} = -p$$



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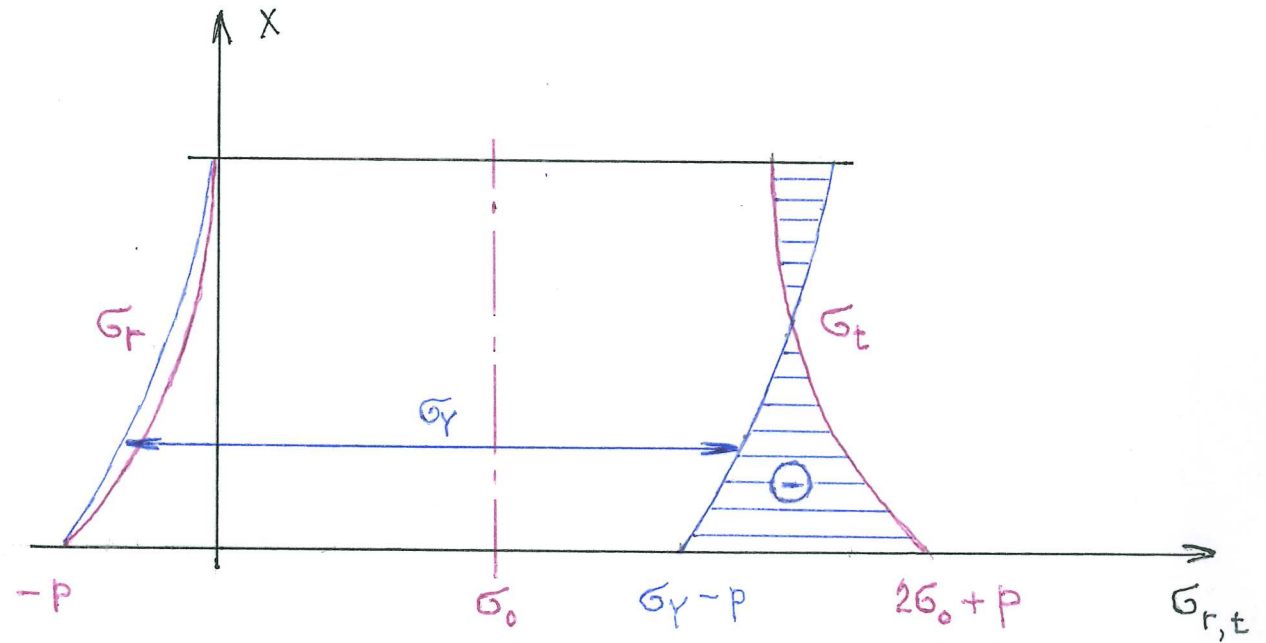
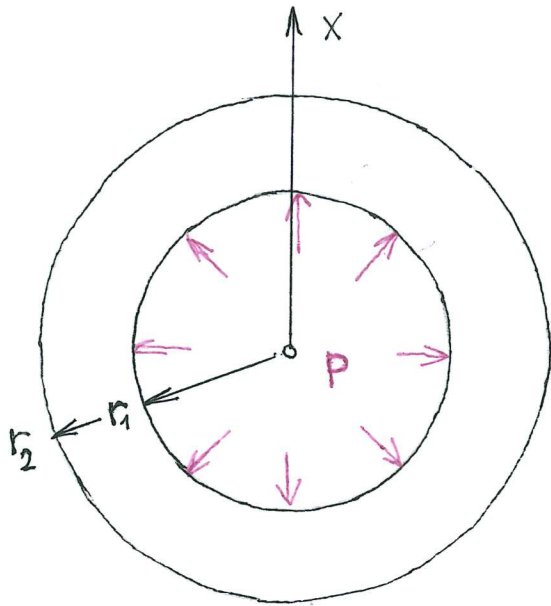
$$\sigma_r(r_1) = \sigma_Y \ln \frac{r_1}{r_2} = -p \equiv -p_p$$

Critical pressure

$$p = \sigma_Y \ln \frac{r_2}{r_1}$$



# Thick wall tube - PMD Example Manual



$$\sigma_r^{\text{res}}(r_1) = -p - (-p) = 0 \quad \Rightarrow \quad \tau_e^{\text{res}} = \sigma_t^{\text{res}} - \sigma_r^{\text{res}} = \sigma_t^{\text{res}} \quad (\text{at } r_1)$$

$$\sigma_t^{\text{res}}(r_1) = \sigma_\gamma - p - (2\sigma_0 + p) = \sigma_\gamma - 2(\sigma_0 + p)$$



# Thick wall tube (3/3)

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Residual stress

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where

$$\sigma_o = \frac{pr_1^2}{r_2^2 - r_1^2} \quad \text{and} \quad p = \sigma_Y \ln \frac{r_2}{r_1}$$



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Shakedown condition

$$\kappa = \frac{2r_2^2}{r_2^2 - r_1^2} \ln \frac{r_2}{r_1} \leq 2 \quad \Rightarrow \quad \frac{r_2}{r_1} < 2.2$$

(verify by direct computation)





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Applications: autofrettage, shot peening, laser shock peening.